

## ROUND HEAD SCREW FOR PLATES

### SCREW FOR PERFORATED PLATES

Cylindrical shoulder designed for fastening metal elements. Achieves an interlocking effect with the hole in the plate, thus guaranteeing excellent static performance.

### STATICS

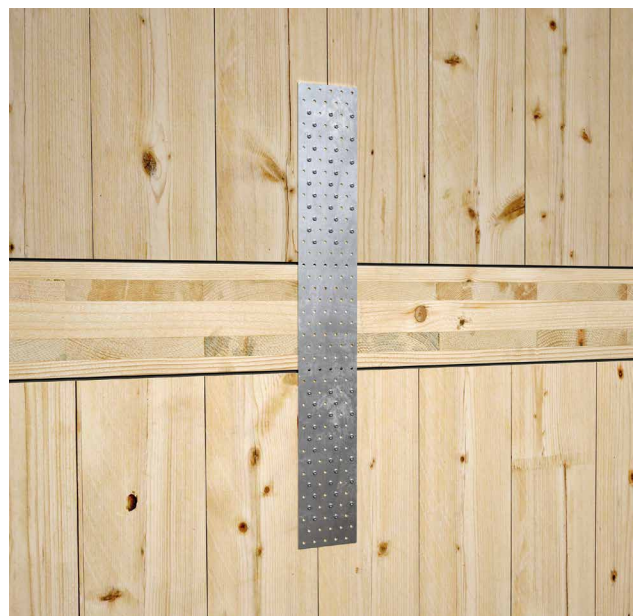
These can be calculated according to Eurocode 5 under thick steel-timber plate connections, even with thin metal elements. Excellent shear strength values.

### NEW-GENERATION WOODS

Tested and certified for use on a wide variety of engineered timbers such as CLT, GL, LVL, OSB and Beech LVL. The LBS5 version up to a length of 40 mm is approved completely without pre-drilling hole on Beech LVL.

### DUCTILITY

Excellent ductility behaviour as evidenced by SEISMIC-REV cyclic tests according to EN 12512.



#### DIAMETER [mm]

3,5 ☒ 5 ☐ 7 ☐ 12

#### LENGTH [mm]

25 ☒ 100 ☐ 200

#### SERVICE CLASS

☒ SC1 ☒ SC2

#### ATMOSPHERIC CORROSIVITY

☒ C1 ☒ C2

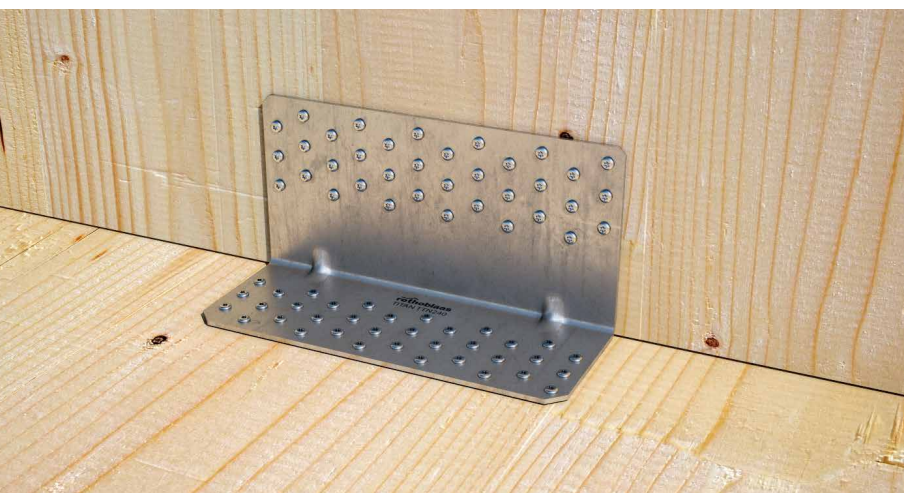
#### WOOD CORROSIVITY

☒ T1 ☒ T2

#### MATERIAL

**Zn**  
ELECTRO  
PLATED

electrogalvanized carbon steel



### FIELDS OF USE

- timber based panels
- solid timber
- glulam (Glued Laminated Timber)
- CLT and LVL
- high density woods

## CODES AND DIMENSIONS

$d_1$ [mm]	CODE	L [mm]	b [mm]	pcs
5 TX 20	LBS525	25	21	500
	LBS540	40	36	500
	LBS550	50	46	200
	LBS560	60	56	200
	LBS570	70	66	200
7 TX 30	LBS760	60	55	100
	LBS780	80	75	100
	LBS7100	100	95	100

## LBS HARDWOOD EVO

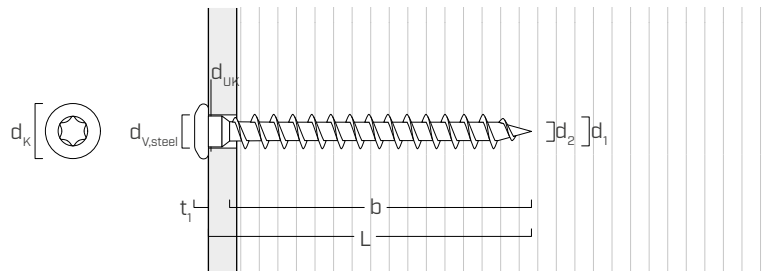
ROUND HEAD SCREW FOR PLATES ON HARDWOODS



DIAMETER [mm]	3	5	7	12
LENGTH [mm]	25	60	200	200

Also available in the LBS HARDWOOD EVO version, L from 80 to 200 mm, diameter Ø5 and Ø7 mm, see page 244.

## GEOMETRY AND MECHANICAL CHARACTERISTICS



### GEOMETRY

Nominal diameter	$d_1$	[mm]	5	7
Head diameter	$d_K$	[mm]	7,80	11,00
Thread diameter	$d_2$	[mm]	3,00	4,40
Underhead diameter	$d_{UK}$	[mm]	4,90	7,00
Head thickness	$t_1$	[mm]	2,40	3,50
Hole diameter on steel plate	$d_{V,steel}$	[mm]	5,0÷5,5	7,5÷8,0
Pre-drilling hole diameter <sup>(1)</sup>	$d_{V,S}$	[mm]	3,0	4,0
Pre-drilling hole diameter <sup>(2)</sup>	$d_{V,H}$	[mm]	3,5	5,0

<sup>(1)</sup> Pre-drilling valid for softwood.

<sup>(2)</sup> Pre-drilling valid for hardwood and beech LVL.

### CHARACTERISTIC MECHANICAL PARAMETERS

Nominal diameter	$d_1$	[mm]	5	7
Tensile strength	$f_{tens,k}$	[kN]	7,9	15,4
Yield moment	$M_{y,k}$	[Nm]	5,4	14,2

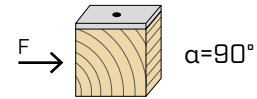
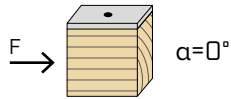
			softwood (softwood)	LVL softwood (LVL softwood)	pre-drilled beech LVL (beech LVL predrilled)	LVL beech <sup>(3)</sup> (beech LVL)
Characteristic withdrawal-resistance parameter	$f_{ax,k}$	[N/mm <sup>2</sup> ]	11,7	15,0	29,0	42,0
Characteristic head-pull-through parameter	$f_{head,k}$	[N/mm <sup>2</sup> ]	10,5	20,0	-	-
Associated density	$\rho_a$	[kg/m <sup>3</sup> ]	350	500	730	730
Calculation density	$\rho_k$	[kg/m <sup>3</sup> ]	≤ 440	410 ÷ 550	590 ÷ 750	590 ÷ 750

<sup>(3)</sup>Valid for  $d_1 = 5$  mm and  $l_{ef} \leq 34$  mm

For applications with different materials please see ETA-11/0030.

## MINIMUM DISTANCES FOR SHEAR LOADS | STEEL-TO-TIMBER

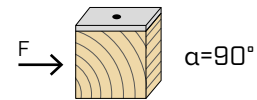
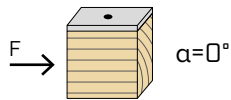
 screws inserted **WITHOUT** pre-drilled hole  $\rho_k \leq 420 \text{ kg/m}^3$



$d_1$	[mm]	5	7
$a_1$	[mm]	$12 \cdot d - 0,7$	42
$a_2$	[mm]	$5 \cdot d - 0,7$	18
$a_{3,t}$	[mm]	$15 \cdot d$	75
$a_{3,c}$	[mm]	$10 \cdot d$	50
$a_{4,t}$	[mm]	$5 \cdot d$	25
$a_{4,c}$	[mm]	$5 \cdot d$	25

$d_1$	[mm]	5	7
$a_1$	[mm]	$5 \cdot d - 0,7$	18
$a_2$	[mm]	$5 \cdot d - 0,7$	18
$a_{3,t}$	[mm]	$10 \cdot d$	50
$a_{3,c}$	[mm]	$10 \cdot d$	50
$a_{4,t}$	[mm]	$10 \cdot d$	50
$a_{4,c}$	[mm]	$5 \cdot d$	25

 screws inserted **WITH** pre-drilled hole



$d_1$	[mm]	5	7
$a_1$	[mm]	$5 \cdot d - 0,7$	18
$a_2$	[mm]	$3 \cdot d - 0,7$	11
$a_{3,t}$	[mm]	$12 \cdot d$	60
$a_{3,c}$	[mm]	$7 \cdot d$	35
$a_{4,t}$	[mm]	$3 \cdot d$	15
$a_{4,c}$	[mm]	$3 \cdot d$	15

$d_1$	[mm]	5	7
$a_1$	[mm]	$4 \cdot d - 0,7$	14
$a_2$	[mm]	$4 \cdot d - 0,7$	14
$a_{3,t}$	[mm]	$7 \cdot d$	35
$a_{3,c}$	[mm]	$7 \cdot d$	35
$a_{4,t}$	[mm]	$7 \cdot d$	35
$a_{4,c}$	[mm]	$3 \cdot d$	15

$\alpha$  = load-to-grain angle

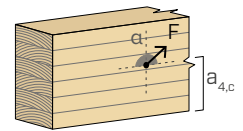
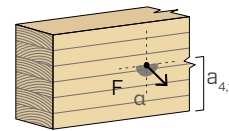
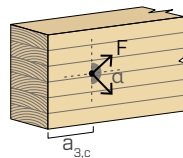
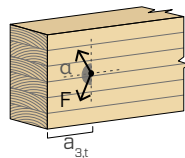
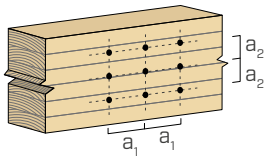
$d = d_1$  = nominal screw diameter

stressed end  
 $-90^\circ < \alpha < 90^\circ$

unloaded end  
 $90^\circ < \alpha < 270^\circ$

stressed edge  
 $0^\circ < \alpha < 180^\circ$

unload edge  
 $180^\circ < \alpha < 360^\circ$



### NOTES

- The minimum distances comply with the EN 1995:2014 standard in accordance with ETA-11/0030.
- In the case of timber-to-timber joints, the minimum spacing ( $a_1$ ,  $a_2$ ) can be multiplied by a coefficient of 1,5.
- In the case of joints with elements in Douglas fir (*Pseudotsuga menziesii*), the minimum spacing and distances parallel to the grain must be multiplied by a coefficient of 1,5.

## EFFECTIVE NUMBER FOR SHEAR LOADS

The load-bearing capacity of a connection made with several screws, all of the same type and size, may be lower than the sum of the load-bearing capacities of the individual connection system.

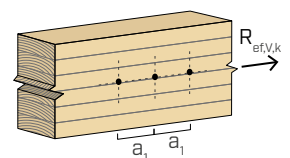
For a row of  $n$  screws arranged parallel to the direction of the grain at a distance  $a_1$ , the characteristic effective load-bearing capacity is equal to:

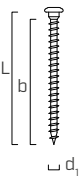
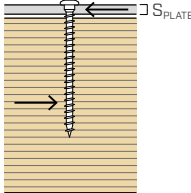
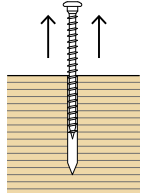
$$R_{ef,V,k} = n_{ef} \cdot R_{V,k}$$

The  $n_{ef}$  value is given in the table below as a function of  $n$  and  $a_1$ .

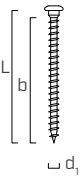
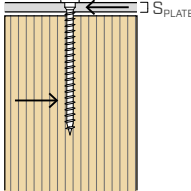
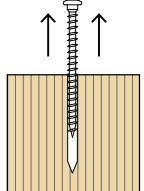
$n$		$a_1^{(*)}$									
		4·d	5·d	6·d	7·d	8·d	9·d	10·d	11·d	12·d	≥ 14·d
2	2	1,41	1,48	1,55	1,62	1,68	1,74	1,80	1,85	1,90	2,00
	3	1,73	1,86	2,01	2,16	2,28	2,41	2,54	2,65	2,76	3,00
	4	2,00	2,19	2,41	2,64	2,83	3,03	3,25	3,42	3,61	4,00
	5	2,24	2,49	2,77	3,09	3,34	3,62	3,93	4,17	4,43	5,00

(\*)For intermediate  $a_1$  values a linear interpolation is possible.

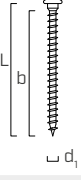
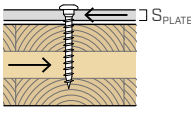
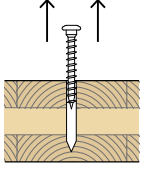


			SHEAR								TENSION
geometry			steel-to-timber $\varepsilon=90^\circ$								thread withdrawal $\varepsilon=90^\circ$
											
$d_1$ [mm]	L [mm]	b [mm]	$R_{V,90,k}$ [kN]								$R_{ax,90,k}$ [kN]
$S_{PLATE}$			1,5 mm	2,0 mm	2,5 mm	3,0 mm	4,0 mm	5,0 mm	6,0 mm	-	
5	25	21	1,59	1,58	1,56	-	-	-	-	1,33	
	40	36	2,24	2,24	2,24	2,24	2,23	2,18	2,13	2,27	
	50	46	2,39	2,39	2,39	2,39	2,39	2,38	2,36	2,90	
	60	56	2,55	2,55	2,55	2,55	2,55	2,54	2,52	3,54	
	70	66	2,71	2,71	2,71	2,71	2,71	2,69	2,68	4,17	
$S_{PLATE}$			3,0 mm	4,0 mm	5,0 mm	6,0 mm	8,0 mm	10,0 mm	12,0 mm	-	
7	60	55	2,81	2,98	3,37	3,80	4,18	4,05	3,92	4,86	
	80	75	3,80	3,88	4,13	4,40	4,63	4,59	4,55	6,63	
	100	95	4,25	4,38	4,63	4,87	5,08	5,03	4,99	8,40	

$\varepsilon$  = screw-to-grain angle

			SHEAR								TENSION
geometry			steel-to-timber $\varepsilon=0^\circ$								thread withdrawal $\varepsilon=0^\circ$
											
$d_1$ [mm]	L [mm]	b [mm]	$R_{V,0,k}$ [kN]								$R_{ax,0,k}$ [kN]
$S_{PLATE}$			1,5 mm	2,0 mm	2,5 mm	3,0 mm	4,0 mm	5,0 mm	6,0 mm	-	
5	25	21	0,77	0,77	0,77	0,76	0,76	0,75	0,74	0,40	
	40	36	0,98	0,98	0,97	0,96	0,95	0,94	0,92	0,68	
	50	46	1,15	1,15	1,14	1,13	1,12	1,10	1,09	0,87	
	60	56	1,32	1,32	1,32	1,32	1,30	1,28	1,27	1,06	
	70	66	1,37	1,37	1,37	1,37	1,37	1,36	1,36	1,25	
$S_{PLATE}$			3,0 mm	4,0 mm	5,0 mm	6,0 mm	8,0 mm	10,0 mm	12,0 mm	-	
7	60	55	1,12	1,21	1,41	1,60	1,77	1,73	1,69	1,46	
	80	75	1,52	1,61	1,83	2,04	2,22	2,17	2,13	1,99	
	100	95	1,91	1,99	2,17	2,35	2,53	2,52	2,51	2,52	

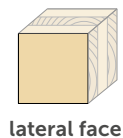
$\varepsilon$  = screw-to-grain angle

geometry			SHEAR								TENSION
			steel-to-CLT lateral face								thread withdrawal lateral face
											
d <sub>1</sub> [mm]	L [mm]	b [mm]	R <sub>V,90,k</sub> [kN]								R <sub>ax,90,k</sub> [kN]
S <sub>PLATE</sub>			1,5 mm	2,0 mm	2,5 mm	3,0 mm	4,0 mm	5,0 mm	6,0 mm	-	
5	25	21	1,48	1,47	1,45	1,44	1,42	1,38	1,35	1,23	
	40	36	2,12	2,12	2,10	2,09	2,05	2,01	1,96	2,11	
	50	46	2,26	2,26	2,26	2,26	2,26	2,25	2,23	2,69	
	60	56	2,41	2,41	2,41	2,41	2,41	2,39	2,38	3,28	
	70	66	2,56	2,56	2,56	2,56	2,56	2,54	2,53	3,86	
S <sub>PLATE</sub>			3,0 mm	4,0 mm	5,0 mm	6,0 mm	8,0 mm	10,0 mm	12,0 mm	-	
7	60	55	2,55	2,77	3,13	3,53	3,86	3,74	3,62	4,50	
	80	75	3,45	3,59	3,82	4,10	4,38	4,33	4,29	6,14	
	100	95	4,00	4,12	4,36	4,58	4,79	4,74	4,70	7,78	

NOTES and GENERAL PRINCIPLES on page 233.

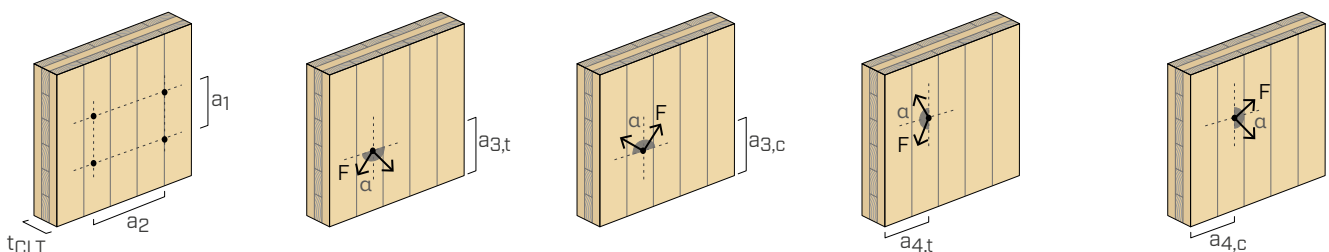
## ■ MINIMUM DISTANCES FOR SHEAR AND AXIAL LOADS | CLT

● screws inserted **WITHOUT** pre-drilled hole



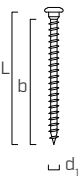
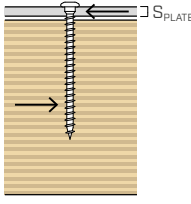
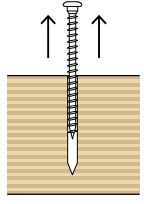
d <sub>1</sub> [mm]		5	7
a <sub>1</sub> [mm]	4·d	20	28
a <sub>2</sub> [mm]	2,5·d	13	18
a <sub>3,t</sub> [mm]	6·d	30	42
a <sub>3,c</sub> [mm]	6·d	30	42
a <sub>4,t</sub> [mm]	6·d	30	42
a <sub>4,c</sub> [mm]	2,5·d	13	18

d = d<sub>1</sub> = nominal screw diameter



### NOTES

- The minimum distances are compliant with ETA-11/0030 and are to be considered valid unless otherwise specified in the technical documents for the CLT panels.
- Minimum distances are valid for minimum CLT thickness  $t_{CLT,min} = 10 \cdot d_1$ .

			SHEAR								TENSION
geometry			steel-LVL								thread withdrawal flat
											
d <sub>1</sub>	L	b	R <sub>V,90,k</sub> [kN]								R <sub>ax,90,k</sub> [kN]
S <sub>PLATE</sub>			1,5 mm	2,0 mm	2,5 mm	3,0 mm	4,0 mm	5,0 mm	6,0 mm	-	
5	25	21	1,59	1,58	1,56	-	-	-	-	1,33	
	40	36	2,24	2,24	2,24	2,24	2,23	2,18	2,13	2,27	
	50	46	2,39	2,39	2,39	2,39	2,39	2,38	2,36	2,90	
	60	56	2,55	2,55	2,55	2,55	2,55	2,54	2,52	3,54	
	70	66	2,71	2,71	2,71	2,71	2,71	2,69	2,68	4,17	
S <sub>PLATE</sub>			3,0 mm	4,0 mm	5,0 mm	6,0 mm	8,0 mm	10,0 mm	12,0 mm	-	
7	60	55	2,81	2,98	3,37	3,80	4,18	4,05	3,92	4,86	
	80	75	3,80	3,88	4,13	4,40	4,63	4,59	4,55	6,63	
	100	95	4,25	4,38	4,63	4,87	5,08	5,03	4,99	8,40	

## STRUCTURAL VALUES

### GENERAL PRINCIPLES

- Characteristic values comply with the EN 1995:2014 standard in accordance with ETA-11/0030.
- Design values can be obtained from characteristic values as follows:

$$R_d = \frac{R_k \cdot k_{mod}}{\gamma_M}$$

The coefficients  $\gamma_M$  and  $k_{mod}$  should be taken according to the current regulations used for the calculation.

- For the mechanical resistance values and the geometry of the screws, reference was made to ETA-11/0030.
- Sizing and verification of the timber elements and metal plates must be done separately.
- The characteristic shear resistances are calculated for screws inserted without pre-drilling hole. In the case of screws inserted with pre-drilling hole, greater resistance values can be obtained.
- The screws must be positioned in accordance with the minimum distances.
- The thread withdrawal characteristic strength has been evaluated considering a fixing length equal to  $b$ .
- The characteristic shear-strength value for LBS Ø5 nails has been evaluated assuming a plate thickness =  $S_{PLATE}$ , always considering the case of thick plate according to ETA-11/0030 ( $S_{PLATE} \geq 1,5$  mm).
- The characteristic shear-strength value for LBS Ø7 screws has been evaluated assuming a plate thickness =  $S_{PLATE}$ , and considering the thin ( $S_{PLATE} \leq 3,5$  mm) intermediate ( $3,5$  mm  $< S_{PLATE} < 7,0$  mm) or thick ( $S_{PLATE} \geq 7$  mm) plate case.
- In the case of combined shear and tensile stress, the following verification must be satisfied:

$$\left( \frac{F_{V,d}}{R_{V,d}} \right)^2 + \left( \frac{F_{ax,d}}{R_{ax,d}} \right)^2 \leq 1$$

- In the case of steel-to-timber connections with a thick plate, it is necessary to assess the effects of timber deformation and install the connectors according to the assembly instructions.

### NOTES | TIMBER

- The characteristic steel-timber shear strengths were evaluated considering both an  $\epsilon$  angle of 90° ( $R_{V,90,k}$ ) and 0° ( $R_{V,0,k}$ ) between the grains of the timber element and the connector.
- Characteristic timber-to-timber shear strengths can be found on page 237.
- The characteristic thread withdrawal resistances were evaluated considering both an  $\epsilon$  angle of 90° ( $R_{ax,90,k}$ ) and of 0° ( $R_{ax,0,k}$ ) between the grains and the connector.

- For the calculation process a timber characteristic density  $\rho_k = 385$  kg/m<sup>3</sup> has been considered. For different values of  $\rho_k$ , the strength values in the table (timber-to-timber shear, steel-to-timber shear and tensile) can be converted by means of the coefficient  $k_{dens}$ :

$$R'_{V,k} = k_{dens,v} \cdot R_{V,k}$$

$$R'_{ax,k} = k_{dens,ax} \cdot R_{ax,k}$$

$\rho_k$ [kg/m <sup>3</sup> ]	350	380	<b>385</b>	405	425	430	440
C-GL	C24	C30	GL24h	GL26h	GL28h	GL30h	GL32h
k <sub>dens,v</sub>	0,90	0,98	1,00	1,02	1,05	1,05	1,07
k <sub>dens,ax</sub>	0,92	0,98	1,00	1,04	1,08	1,09	1,11

Strength values thus determined may differ, for higher safety standards, from those resulting from an exact calculation.

### NOTES | CLT

- The characteristic values are according to the national specifications ÖNORM EN 1995 - Annex K.
- For the calculation process a mass density  $\rho_k = 350$  kg/m<sup>3</sup> has been considered for CLT elements.
- The characteristics shear resistance are calculated considering a minimum fixing length of 4  $d_1$ .
- The characteristic shear strength is independent from the direction of the grain of the CLT panels outer layer.
- The axial thread withdrawal strength is valid for minimum CLT thickness  $t_{CLT,min} = 10 \cdot d_1$ .

### NOTES | LVL

- For the calculation process a mass density equal to  $\rho_k = 480$  kg/m<sup>3</sup> has been considered for softwood LVL elements.
- The axial thread-withdrawal resistance was calculated considering a 90° angle between the grains and the connector.
- The characteristic shear strengths are evaluated for connectors inserted on the side face (wide face) considering, for individual timber elements, a 90° angle between the connector and the grain, a 90° angle between the connector and the side face of the LVL element and a 0° angle between the force and the grain.